

# Zero-Drift, Rail-to-Rail I/O CMOS Operational Amplifiers

## 1 FEATURES

- **Low Offset Voltage:**  $\pm 1\mu\text{V}$  (TYP)
- **Input Offset Drift:**  $0.1\mu\text{V}/^\circ\text{C}$
- **High Gain Bandwidth Product:** 5MHz
- **Rail-to-Rail Input and Output**
- **High Gain, CMRR, PSRR:** 130dB
- **High Slew Rate:** 3.4V/us
- **Low Noise:** 0.8uVp-p (0.1Hz ~ 10Hz)
- **Low Power Consumption:** 730uA /op amp
- **Overload Recovery Time:** 1us
- **Low Supply Voltage:** +2.7V to +5.5V
- **No External Capacitors Required**
- **Extended Temperature:** -40°C to +125°C

## 2 APPLICATIONS

- **Temperature Sensors**
- **Medical/ Industrial Instrumentation**
- **Pressure Sensors**
- **Battery-Powered Instrumentation**
- **Active Filtering**
- **Weight Scale Sensor**
- **Strain Gage Amplifiers**
- **Power Converter/ Inverter**

## 3 DESCRIPTIONS

The RS8581 series of CMOS operational amplifiers use auto-zero techniques to simultaneously provide very low offset voltage (5uV max) and near-zero drift over time and temperature. This family of amplifiers has ultralow noise, offset and power.

This miniature, high-precision operational amplifiers offset high input impedance and rail-to-rail input and rail-to-rail output swing. With high gain-bandwidth product of 5MHz and slew rate of 3.4V/us.

Single or dual supplies as low as +2.7V ( $\pm 1.35\text{V}$ ) and up to +5.5V ( $\pm 2.75\text{V}$ ) may be used.

The RS8581 are specified for the extended industrial and automotive temperature range (-40°C to 125°C). The RS8581 single amplifier is available in 5-lead SOT23 packages.

**Device Information<sup>(1)</sup>**

PART NUMBER	PACKAGE	BODY SIZE (NOM)
RS8581	SOT23-5	2.92mm×1.62mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.

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## 4 Revision History

Note: Page numbers for previous revisions may differ from page numbers in the current version.

VERSION	Change Date	Change Item
A.1	2023/1/18	Initial version completed

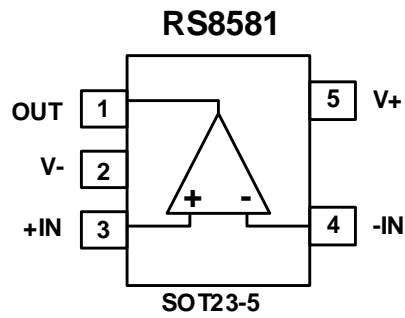
**5 PACKAGE/ORDERING INFORMATION <sup>(1)</sup>**

Orderable Device	Package Type	Pin	Channel	Op Temp (°C)	Device Marking <sup>(2)</sup>	Package Qty
RS8581TXF	SOT23-5	5	1	-40°C ~125°C	8581	Tape and Reel,3000

## NOTE:

- (1) This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the right-hand navigation.
- (2) There may be additional marking, which relates to the lot trace code information (data code and vendor code), the logo or the environmental category on the device.

## 6 Pin Configuration and Functions (Top View)



### Pin Description

NAME	PIN	I/O <sup>(1)</sup>	DESCRIPTION
	SOT23-5		
-IN	4	I	Negative (inverting) input
+IN	3	I	Positive (noninverting) input
OUT	1	O	Output
V-	2	-	Negative (lowest) power supply
V+	5	-	Positive (highest) power supply

(1) I = Input, O = Output.

## 7 SPECIFICATIONS

### 7.1 Absolute Maximum Ratings

Over operating free-air temperature range (unless otherwise noted) <sup>(1)</sup>

		MIN	MAX	UNIT
Voltage	Supply, $V_S=(V+) - (V-)$		6	V
	Signal input pin <sup>(2)</sup>	(V-)-0.5	(V+) +0.5	
	Signal output pin <sup>(3)</sup>	(V-)-0.5	(V+) +0.5	
Current	Signal input pin <sup>(2)</sup>	-10	10	mA
	Signal output pin <sup>(3)</sup>	-55	55	mA
	Output short-circuit <sup>(4)</sup>	Continuous		
$\theta_{JA}$	Package thermal impedance <sup>(5)</sup>	SOT23-5	230	°C/W
Temperature	Operating range, $T_A$	-40	125	°C
	Junction, $T_J$ <sup>(6)</sup>	-40	150	
	Storage, $T_{stg}$	-65	150	

(1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not implied.

(2) Input terminals are diode-clamped to the power-supply rails. Input signals that can swing more than 0.5V beyond the supply rails should be current-limited to 10mA or less.

(3) Output terminals are diode-clamped to the power-supply rails. Output signals that can swing more than 0.5V beyond the supply rails should be current-limited to  $\pm 55$ mA or less.

(4) Short-circuit to ground, one amplifier per package.

(5) The package thermal impedance is calculated in accordance with JESD-51.

(6) The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $R_{\theta JA}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} - T_A) / R_{\theta JA}$ . All numbers apply for packages soldered directly onto a PCB.

### 7.2 ESD Ratings

The following ESD information is provided for handling of ESD-sensitive devices in an ESD protected area only.

		VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	$\pm 2000$
		Charged-device model (CDM), per ANSI/ESDA/JEDEC JS-002 <sup>(2)</sup>	$\pm 1500$
		Machine Model (MM)	$\pm 200$

(1) JEDEC document JEP155 states that 500 V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250 V CDM allows safe manufacturing with a standard ESD control process.



### ESD SENSITIVITY CAUTION

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### 7.3 Recommended Operating Conditions

Over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
Supply voltage, $V_S= (V+) - (V-)$	Single-supply	2.7		5.5	V
	Dual-supply	$\pm 1.35$		$\pm 2.75$	

## 7.4 ELECTRICAL CHARACTERISTICS

(At  $T_A = +25^\circ\text{C}$ ,  $V_S = 5\text{V}$ ,  $R_L = 10\text{k}\Omega$  connected to  $V_S/2$ , and  $V_{OUT} = V_S/2$ , Full =  $-40^\circ\text{C}$  to  $+125^\circ\text{C}$ , unless otherwise noted.)

PARAMETER		CONDITIONS	$T_J$	RS8581			
				MIN <sup>(2)</sup>	TYP <sup>(3)</sup>	MAX <sup>(2)</sup>	UNIT
<b>POWER SUPPLY</b>							
$V_S$	Operating Voltage Range		$25^\circ\text{C}$	2.7		5.5	V
IQ	Quiescent Current/Amplifier	$V_S = \pm 2.5\text{V}$	$25^\circ\text{C}$		730	900	$\mu\text{A}$
PSRR	Power-Supply Rejection Ratio	$V_S = 2.7\text{V}$ to $5.5\text{V}$ , $V_{CM} = V_S/2$	$25^\circ\text{C}$		130		dB
			Full	100			
<b>INPUT</b>							
$V_{OS}$	Input Offset Voltage	$V_{CM} = V_S/2$	$25^\circ\text{C}$	-5	$\pm 1$	5	$\mu\text{V}$
$V_{OS}$ $T_C$	Input Offset Voltage Average Drift		Full		0.1		$\mu\text{V}/^\circ\text{C}$
IB	Input Bias Current	$V_{CM} = V_S/2$	$25^\circ\text{C}$		$\pm 50$		$\mu\text{A}$
$I_{OS}$	Input Offset Current		$25^\circ\text{C}$		$\pm 10$		$\mu\text{A}$
$V_{CM}$	Common-Mode Voltage Range		$25^\circ\text{C}$	(V-) - 0.1		(V+) + 0.1	V
CMRR	Common-Mode Rejection Ratio	$(V-) - 0.1\text{V} < V_{CM} < (V+) + 0.1\text{V}$	$25^\circ\text{C}$		130		dB
			Full	100			
<b>OUTPUT</b>							
$A_{OL}$	Open-Loop Voltage Gain	$R_L = 10\text{k}\Omega$ , $V_O = 0.3\text{V}$ to $4.7\text{V}$	$25^\circ\text{C}$		130		dB
			Full	110			
$V_{OH}$	Output Voltage High	$R_L = 10\text{k}\Omega$ to GND	$25^\circ\text{C}$	4.98	4.992		V
$V_{OL}$	Output Voltage Low	$R_L = 10\text{k}\Omega$ to V+	$25^\circ\text{C}$		5	15	mV
$I_{OUT}$	Output Short-Circuit Current	$V_S = \pm 2.5\text{V}$ , $V_O = 0\text{V}$	$25^\circ\text{C}$		45		mA
$C_{LOAD}$	Capacitive Load Drive				100		pF
<b>FREQUENCY RESPONSE</b>							
SR	Slew Rate		$25^\circ\text{C}$		3.4		V/ $\mu\text{s}$
GBP	Gain-Bandwidth Product		$25^\circ\text{C}$		5		MHz
PM	Phase Margin	$C_L = 100\text{pF}$	$25^\circ\text{C}$		60		$^\circ$
$t_S$	Setting Time, 0.1%	$V_S = \pm 2.5\text{V}$ , $C_L = 100\text{pF}$	$25^\circ\text{C}$		0.8		$\mu\text{s}$
$t_{OR}$	Overload Recovery Time		$25^\circ\text{C}$		1		$\mu\text{s}$
<b>NOISE</b>							
$E_n$	Input Voltage Noise	$f = 0.1\text{Hz}$ to $10\text{Hz}$ , $V_S = \pm 2.5\text{V}$	$25^\circ\text{C}$		0.8		$\mu\text{V}_{PP}$
$e_n$	Input Voltage Noise Density	$f = 1\text{KHz}$	$25^\circ\text{C}$		35		$\text{nV}/\sqrt{\text{Hz}}$

## 7.5 TYPICAL CHARACTERISTICS

NOTE: The graphs and tables provided following this note are a statistical summary based on a limited number of samples and are provided for informational purposes only.

At  $T_A = +25^\circ\text{C}$ ,  $V_S = 5\text{V}$ ,  $R_L = 10\text{k}\Omega$  connected to  $V_S/2$ ,  $V_{OUT} = V_S/2$ , unless otherwise noted.

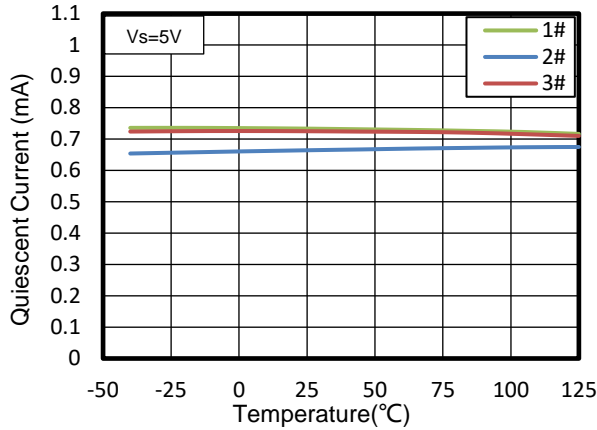


Figure 1. Quiescent Current vs Temperature

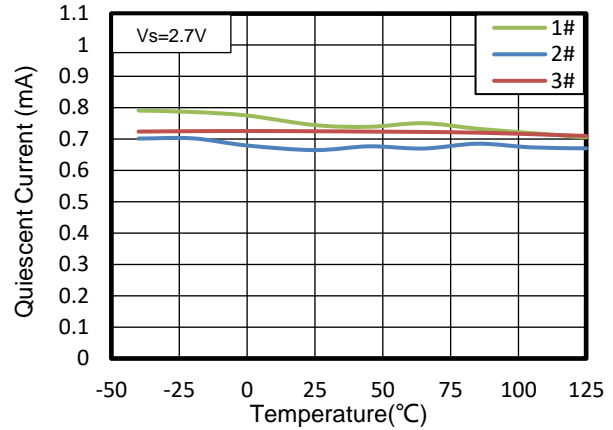


Figure 2. Quiescent Current vs Temperature

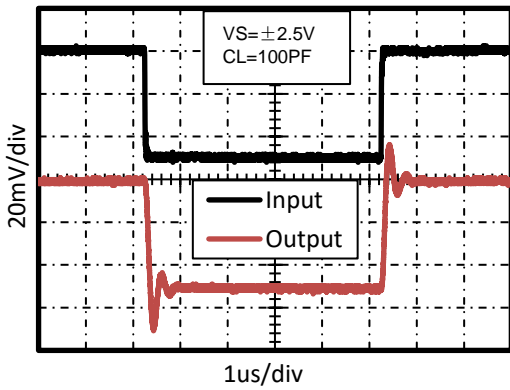


Figure 3. Small-Signal Step Response

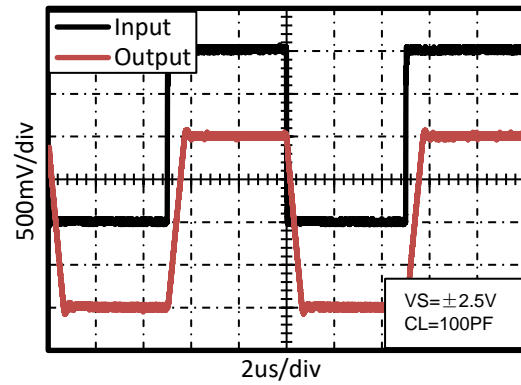


Figure 4. Large-Signal Step Response

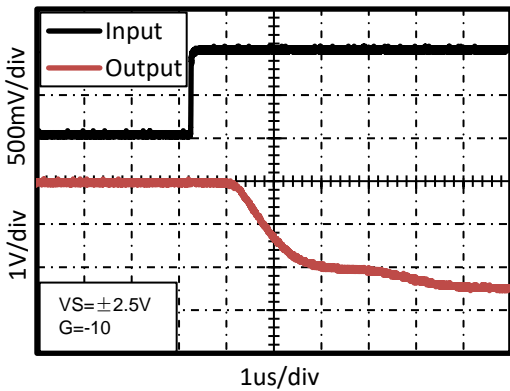


Figure 5. Positive Overtolerance Recovery

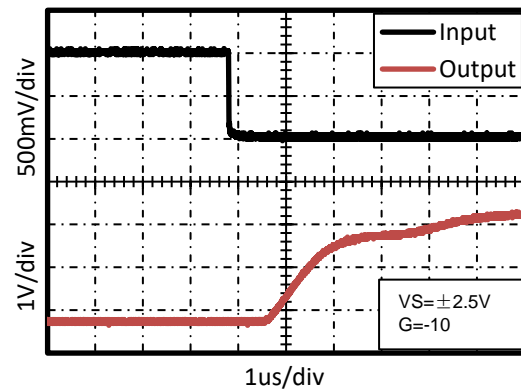


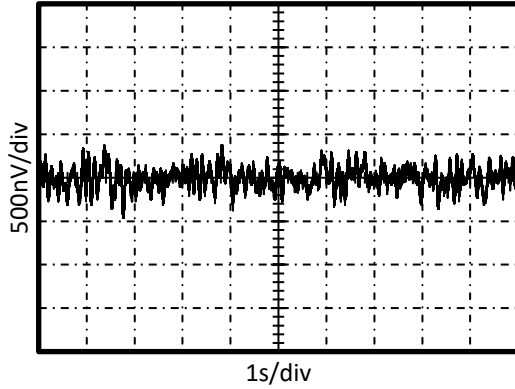
Figure 6. Negative Overtolerance Recovery



## TYPICAL CHARACTERISTICS

NOTE: The graphs and tables provided following this note are a statistical summary based on a limited number of samples and are provided for informational purposes only.

At  $T_A = +25^\circ\text{C}$ ,  $V_S = 5\text{V}$ ,  $R_L = 10\text{k}\Omega$  connected to  $V_S/2$ ,  $V_{OUT} = V_S/2$ , unless otherwise noted.



**Figure 7. 0.1Hz to 10Hz Noise**

## 8 Detailed Description

### 8.1 Overview

The RS8581 series op amps are unity-gain stable and free from unexpected output phase reversal. They use auto-zeroing techniques to provide low offset voltage and very low drift over time and temperature.

Good layout practice mandates use of a 0.1 $\mu$ F capacitor placed closely across the supply pins.

For lowest offset voltage and precision performance, circuit layout and mechanical conditions should be optimized. Avoid temperature gradients that create thermoelectric (Seebeck) effects in thermocouple junctions formed from connecting dissimilar conductors. These thermally-generated potentials can be made to cancel by assuring that they are equal on both input terminals.

- Use low thermoelectric-coefficient connections (avoid dissimilar metals).
- Thermally isolate components from power supplies or other heat-sources.
- Shield op amp and input circuitry from air currents, such as cooling fans.

Following these guidelines will reduce the likelihood of junctions being at different temperatures, which can cause thermoelectric voltages of 0.1 $\mu$ V/ $^{\circ}$ C or higher, depending on materials used.

### 8.2 OPERATING VOLTAGE

The RS8581 series op amps operate over a power-supply range of +2.7V to +5.5V ( $\pm$ 1.35V to  $\pm$ 2.75V). Supply voltages higher than 7V (absolute maximum) can permanently damage the amplifier. Parameters that vary over supply voltage or temperature are shown in the Typical Characteristics section of this data sheet.

## 9 Application and Implementation

Information in the following applications sections is not part of the Runic component specification, and Runic does not warrant its accuracy or completeness. Runic's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

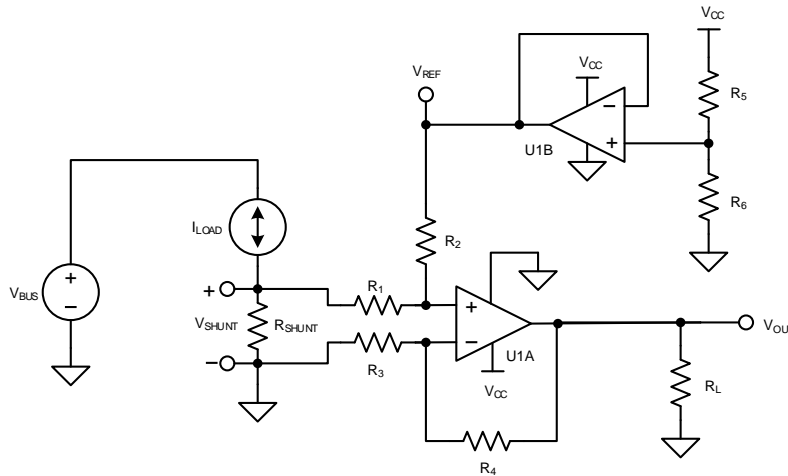
### 9.1 APPLICATION NOTE

The RS8581 is a unity-gain stable, precision operational amplifier with very low offset voltage drift; these devices are also free from output phase reversal. Applications with noisy or high-impedance power supplies require decoupling capacitors close to the device power-supply pins. In most cases, 0.1uF capacitors are adequate.

### Typical Applications

#### 9.2 Bidirectional Current-Sensing

This single-supply, low-side, bidirectional current-sensing solution detects load currents from -1A to 1A. The single-ended output spans from 110mV to 3.19V. This design uses the RS8581 because of its low offset voltage and rail-to-rail input and output. One of the amplifiers is configured as a difference amplifier and the other provides the reference voltage.



**Figure 8. Bidirectional Current-Sensing Schematic**

### 9.3 Design Requirements

This solution has the following requirements:

- Supply voltage: 3.3 V
- Input: -1 A to 1 A
- Output: 1.65 V  $\pm$  1.54 V (110 mV to 3.19 V)

### 9.4 Detailed Design Procedure

The load current,  $I_{LOAD}$ , flows through the shunt resistor ( $R_{SHUNT}$ ) to develop the shunt voltage,  $V_{SHUNT}$ . The shunt voltage is then amplified by the difference amplifier, which consists of U1A and  $R_1$  through  $R_4$ . The gain of the difference amplifier is set by the ratio of  $R_4$  to  $R_3$ . To minimize errors, set  $R_2 = R_4$  and  $R_1 = R_3$ . The reference voltage,  $V_{REF}$ , is supplied by buffering a resistor divider using U1B. The transfer function is given by Equation 1.

$$V_{OUT} = V_{SHUNT} \times \text{Gain}_{\text{Diff\_Amp}} + V_{REF}$$

Where

$$V_{SHUNT} = I_{LOAD} \times R_{SHUNT}$$

$$\text{Gain}_{\text{Diff\_Amp}} = \frac{R_4}{R_3}$$

$$V_{REF} = V_{CC} \times \left( \frac{R_6}{R_5 + R_6} \right)$$

(1)

There are two types of errors in this design: offset and gain. Gain errors are introduced by the tolerance of the shunt resistor and the ratios of  $R_4$  to  $R_3$  and, similarly,  $R_2$  to  $R_1$ . Offset errors are introduced by the voltage divider ( $R_5$  and  $R_6$ ) and how closely the ratio of  $R_4/R_3$  matches  $R_2/R_1$ . The latter value impacts the CMRR of the difference amplifier, which ultimately translates to an offset error. Because this is a low-side measurement, the value of  $V_{SHUNT}$  is the ground potential for the system load. Therefore, it is important to place a maximum value on  $V_{SHUNT}$ . In this design, the maximum value for  $V_{SHUNT}$  is set to 100 mV. Equation 2 calculates the maximum value of the shunt resistor given a maximum shunt voltage of 100 mV and maximum load current of 1 A.

$$R_{SHUNT(Max)} = \frac{V_{SHUNT(Max)}}{I_{LOAD(Max)}} = \frac{100 \text{ mV}}{1 \text{ A}} = 100 \text{ m}\Omega \quad (2)$$

The tolerance of  $R_{SHUNT}$  is directly proportional to cost. For this design, a shunt resistor with a tolerance of 0.5% was selected. If greater accuracy is required, select a 0.1% resistor or better.

The load current is bidirectional; therefore, the shunt voltage range is -100 mV to 100 mV. This voltage is divided down by  $R_1$  and  $R_2$  before reaching the operational amplifier, U1A. Take care to ensure that the voltage present at the noninverting node of U1A is within the common-mode range of the device. Therefore, it is important to use an operational amplifier, such as the RS8581, that has a common-mode range that extends below the negative supply voltage. Finally, to minimize offset error, note that the RS8581 has a typical offset voltage of  $\pm 1\mu\text{V}$  ( $\pm 5\mu\text{V}$  maximum). Given a symmetric load current of -1 A to 1 A, the voltage divider resistors ( $R_5$  and  $R_6$ ) must be equal. To be consistent with the shunt resistor, a tolerance of 0.5% was selected. To minimize power consumption, 10k $\Omega$  resistors were used. To set the gain of the difference amplifier, the common-mode range and output swing of the RS8581 must be considered. Equation 3 and Equation 4 depict the typical common-mode range and maximum output swing, respectively, of the RS8581 given a 3.3V supply.

$$-100\text{mV} < V_{CM} < 3.4\text{V} \quad (3)$$

$$100\text{mV} < V_{OUT} < 3.2\text{V} \quad (4)$$

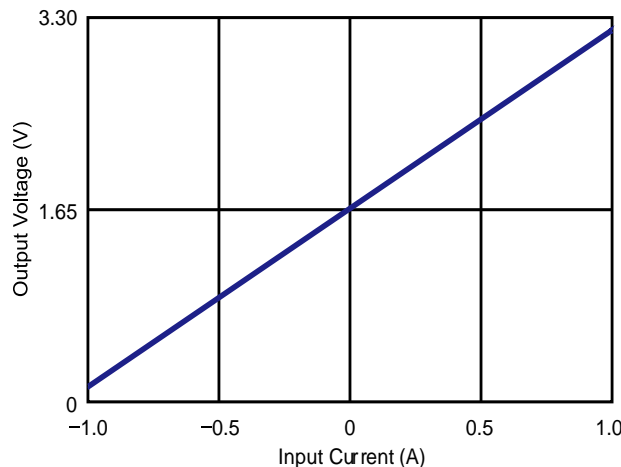
The gain of the difference amplifier can now be calculated as shown in Equation 5.

$$\text{Gain}_{\text{Diff\_Amp}} = \frac{V_{OUT\_Max} - V_{OUT\_Min}}{R_{SHUNT} \times (I_{MAX} - I_{MIN})} = \frac{3.2 \text{ V} - 100 \text{ mV}}{100 \text{ m}\Omega \times [1 \text{ A} - (-1 \text{ A})]} = 15.5 \frac{\text{V}}{\text{V}} \quad (5)$$

The resistor value selected for  $R_1$  and  $R_3$  was 1k $\Omega$ . 15.4k $\Omega$  was selected for  $R_2$  and  $R_4$  because it is the nearest standard value. Therefore, the ideal gain of the difference amplifier is 15.4 V/V.

The gain error of the circuit primarily depends on  $R_1$  through  $R_4$ . As a result of this dependence, 0.1% resistors were selected. This configuration reduces the likelihood that the design requires a two-point calibration. A simple one-point calibration, if desired, removes the offset errors introduced by the 0.5% resistors.

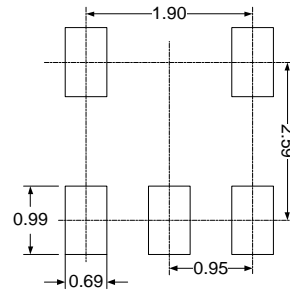
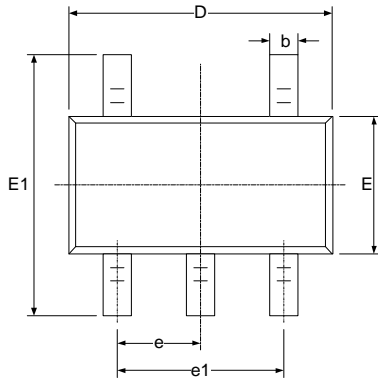
## 9.5 Application Curve



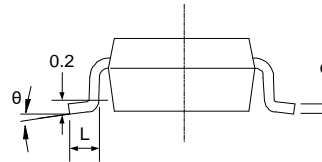
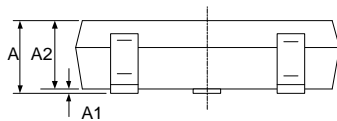
**Figure 9. Bidirectional Current-Sensing Circuit Performance: Output Voltage vs Input Current**

# 10 PACKAGE OUTLINE DIMENSIONS

## SOT23-5



**RECOMMENDED LAND PATTERN (Unit: mm)**



Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	1.050	1.250	0.041	0.049
A1	0.000	0.100	0.000	0.004
A2	1.050	1.150	0.041	0.045
b	0.300	0.500	0.012	0.020
c	0.100	0.200	0.004	0.008
D	2.820	3.020	0.111	0.119
E	1.500	1.700	0.059	0.067
E1	2.650	2.950	0.104	0.116
e	0.950 (BSC)		0.037 (BSC)	
e1	1.800	2.000	0.071	0.079
L	0.300	0.600	0.012	0.024
$\theta$	0°	8°	0°	8°

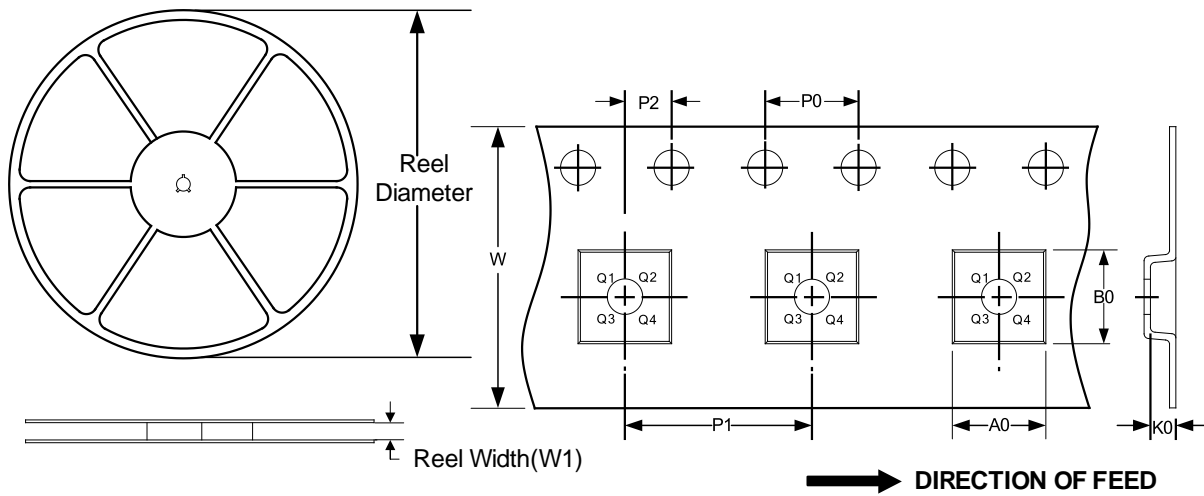
**NOTE:**

- A. All linear dimension is in millimeters.
- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.15 per side.
- D. BSC: Basic Dimension. Theoretically exact value shown without tolerances.

# 11 TAPE AND REEL INFORMATION

## REEL DIMENSIONS

## TAPE DIMENSION



NOTE: The picture is only for reference. Please make the object as the standard.

### KEY PARAMETER LIST OF TAPE AND REEL

Package Type	Reel Diameter	Reel Width (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P0 (mm)	P1 (mm)	P2 (mm)	W (mm)	Pin1 Quadrant
SOT23-5	7"	9.5	3.20	3.20	1.40	4.0	4.0	2.0	8.0	Q3

NOTE:

1. All dimensions are nominal.
2. Plastic or metal protrusions of 0.15mm maximum per side are not included.

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